GURVICH, D.B.; SHEVARDINA, Z.I.

Polarographic method of determining aldehydes in mixed polyvinyl acetals. Plast. massy no.12:55-58 '60. (MIRA 13:12)
(Aldehydes) (Vinyl compounds)

SHEVARDNADZE, M.G.

Mountain forest soils of the Natanebi River basin. Soob.AN Gruz.
SSR 26 no.2:207-212 '61. (MIRA 14:4)

1. Tbilisskiy gosudarstvennyy universitet im. Stalina. Predstavleno akademikom M.N.Sabashvili.
(Natanebi Valley—Forest soils)

SHEVARDNADZE, M.G.

Content of organic matter in the mountain forest soils of Adzharia and Guriya. Trudy Tbil.GU 72:279-294 '59. (MIRA 15:5)
(Adzhar A.S.S.R.—Soils—Analysis) (Guriya—Soils—Analysis)

SHEVARDNADZE, M.G.

Mountain-forest soils of Adzharistan. Trudy Tbil. GU 90:75-88 '63. (MIRA 17:4)

SHEVAREV, P.A.

On the comparative visibility of the protozoal figures. Visual Sensations and Perceptions,M.,1935.

SHEVAREV, P.A.

Generalized associations [with summary in English]. Vop. psikhol. 4 no.1:16-23 Ja-F '58. (MIRA 11:3)

1. Institut psikhologii APN RSFSR, Moskva.
(Association of ideas)

GUR'YANOV, Ye.V.; MENCHINSKAYA, N.A.; SHEVAREV, P.A.

Thirteenth International Congress of Applied Psychology.
Vop.psikhol. 4 no.4:156-162 Jl-Ag '58. (MIRA 11:11)
(Rome--Psychology, Applied--Congresses)

SHEVAREV, P.A.

Psychological analysis of textbook material in the Russian language.
Vop. psikhol. 5 no.3:117-128 My-Je '59. (MIRA 12:9)

1.Institut psikhologii Akademii pedagogicheskikh nauk RSFSR,
Moskva.
(Russian language--Study and teaching)

SHEVAREV, P.A.

Study of the material substratum of mental processes in the investigations of Soviet psychologists. Vop.psikhol. 6 no.2:35-46 Mr-Ap '60. (MIRA 13:7)

1. Institut psikhologii APN RSFSR, Moskva.
(Thought and thinking)
(Senses and sensation)

SHEVAREV, P.A.

Abstracting visually given properties and characteristics of objects.
Vop. psikhol. 7 no.6:63-76 N-D '61. (MIRA 15:1)

1. Institut psikhologii Akademii pedagogicheskikh nauk RSFSR, Moskva.
(Abstraction)

SHEVAREV, P.A.

Basic principles of the theory of set presented by D.N.Uznadze.
Vop. psikhol. 8 no.5:95-106 S-O '62. (MIRA 16:5)

1. Institut psikhologii Akademii pedagogicheskikh nauk RSFSR, Moskva.
(Attitude (Psychology)) (Personality)

SHEVAREVA, T.P.

Bird migrations and their study. Est.v shkole no.1:73-77 Ja-F '54.
(MLRA 6:12)

1. Byuro kol'tsevaniya Upravleniyapo zapovednikam.
(Birds--Migrations)

SHEVAREVA, T. P.

LEBEDEVA, M.; SHEVAREVA, T. P.

What birdbands tell us. IUn. nat. no.4:28-29 Ap '57. (MLRA 10:6)

1. Nauchnyy sotrudnik Byuro kol'tsevaniya.
(Birdbanding)

LEBEDEVA, M.I., nauchnyy sotrudnik,; SHEVAREVA, T.P., nauchnyy sotrudnik

International count of white stork populations. Biol. v shkole no. 3:91 My-Je '58. (MIRA 11:8)

1. Komissiya po okhrane prirody AN SSSR.
(Storks)

SHEVAREVA, T.P.

Some data on the migration of water birds nesting in the northern part of the Soviet Union. Migr.zhiv. no.1:95-123 '59. (MIRA 13:6)

1. Komissiya po okhrane prirody AN SSSR.
(Birds--Migration) (Water birds)

LEBEDEVA, M.I.; SHEVAREVA, T.P.

Migrations of diurnal birds of prey in the U.S.S.R. Migr. zhiv. no. 2:100-127 '60. (MIRA 13:12)

1. Komissiya po okhrane prirody AN SSSR.
(Birds of prey) (Birds--Migration)

SHEVAREVA, T.P.

Longevity of birds in nature (according to the data of banding).
Ornitologiia no.3:48-51 '60. (MIRA 14:6)
(Birds--Age)

LEBEDEVA, M.I.; SHEVAREVA, T.P.

Reasons for the death of birds in nature; according to bird-banding data. Okhr. prir. i zapov. delo v SSSR no. 6:67-83 '60.
(MIRA 14:5)

(Birds)

SHEVAREVA, T.P.

Recent data on the migration of birds in the north of the U.S.S.R. Trudy Probl. i tem. sov. no.9:146-150 '60.
(MIRA 13:9)

1. Byuro kol'tsevaniya Akademii nauk SSSR.
(Russia, Northern--Birds--Migration)

SAPETIN, Ya.V.; SHEVAREVA, T.P.

Distribution of ducks and coots nesting in the U.S.S.R. in different wintering places. Ornitologiia no.2:271-275 '59.
(MIRA 14:7)

(Ducks) (Coots)

SHEVAREVA, T.P.

New data on the occurrence of ringed Caspian terns (Hydroprogne tschegrava Lepechin). Migr. zhiv. no.3:92-105 '62. (MIRA 16:2)

1. Komissiya po okhrane prirody pri Gosplane SSSR.
(Terns)
(Birds—Migration)

SHEVAREVA, T.P.; SAPETIN, Ya.V.

Population of bank swallows in the Oka Valley based on the birdbanding data. Trudy OGZ no.4:337-348 '62. (MIRA 17:9)

SHEVAREVA, T.P.

Population characteristics of the migration of birds. Ornitologiia no.7:318-327 '65. (MIRA 18:10)

SHEVARIKHIN, I.

The commission visits a workshop. Okhr. truda i sots. strakh. 4 no.7:15 Jl '61. (MIRA 14:7)

1. Predsedatel' zavkoma Feodosiyskogo zavoda pod"yemno-transportnogo oborudovaniya.
(Fedodosiya--Machinery industry--Hygienic aspects)

SHEVARKOV, N.A.

How we organized topical school clubs. Geog.v shkole 19 no.2: 59-60 Mr-Ap '56. (MIRA 9:7)

1.Shkola no.18 g. Stalinnogorska.
(Geography--Study and teaching)

SHEVARKOV, N.A.

My suggestions. Geog. v shkole 22 no.1:45-49 Ja-F '59.
(MIRA 12:4)

1. Srednyaya shkola No.18, Stalinogorsk.
(Geography--Study and teaching)

SHARKOVA, Ye.F.; VIRNIK, A.D.; ROGOVIN, Z.A.; Prinimala uchastiye:
SHIVAROVA, K.K.

Polymer analog conversions of a graft copolymer of cellulose and polyglycidyl methacrylate. Vysokom.soed. 6 no. 5:951-956 My '64. (MIRA 17:6)

1. Moskovskiy tekstil'nyy institut.

SOV/130-58-8-6/18

AUTHORS: Chikalenko, G.A. and Shevbunov, E.V.

TITLE: Influence of Pouring Conditions on the Quality of 5-6-ton Plate Ingots and the Quality of Plates Rolled From Them (Vliyaniye usloviy otlivki na kachestvo listovykh 5-6-t slitkov i prokatannykh iz nikh listov)

PERIODICAL: Metallurg, 1958, Nr 8, pp 14 - 16 (USSR)

ABSTRACT: At the imeni Il'ich Works, 5-6 ton plate ingots of carbon and boiler steel are bottom-poured in big-end-up moulds with two feeders in their bottoms (Figure 1) and hot tops. The metal is poured from 130-ton ladles through 40-45 mm diameter nozzles, there being 4 moulds to a stool and a hot-top mixture being used, With the previously used diffuser shape of nozzle in the ingot-mould feeder (Figure 2a) defects associated with early crust formation in the metal occur. It was found that the use of a cylindrical nozzle (Figure 2b) reduced the incidence of such defects in the ingots (Table 1) and in plates rolled from them (Table 2). Improvements were

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SOV/130-58-8-6/18

Influence of Pouring Conditions on the Quality of 5-6 ton Plate Ingots and the Quality of Plates Rolled From Them

also observed in the tendency to lamination in plate edges (Table 3).
There are 2 figures and 3 tables.

Card 2/2

1. Steel--Production 2. Steel--Processing 3. Steel--Quality control 4. Steel plates--Quality control

SHEVCHAK, G.

Operator suggests improvements. Izobr. i rats. no.6:21 Je '61.
(MIRA 14:6)

1. Redaktor Instituta nauchno-tekhnicheskoy informatsii i propagandy BSSR, g. Minsk.
(Minsk--Excavating machinery--Technological innovations)

BOGDANOVICH, Boris Mikhaylovich, kand. tekhn. nauk; PROKHORENKO,
V.K., spets. red.; SHEVCHAK, G.I., red.

[Fundamentals of the theory of the design of transistor radio receivers with low noise coefficients] Osnovy teorii i rascheta tranzistornykh radiopriemnikov s malym koeffitsientom shuma. Minsk, Nauchno-tekhn. ob-vo radiotekhniki i elektrosviazi im. A.S.Popova, 1962. 69 p. (MIRA 17:3)

ANISHCHENKO, Andrey Fedorovich; SHEVCHAK, G.I., red.

[Structural mechanics; a textbook for engineers and builders] Stroitel'naia mekhanika; uchebno-metodicheskoe posobie dlia inzhenerov-stroitelei. Minsk, Vysshaia shkola, 1965. 46 p. (MIRA 18:11)

SHEVCHNEKO, A., inzhener; PARAD, S., inzhener.

The productivity of the unit has increased. Prom.koop. no.11; 27-29 N '55. (MLRA 9:5)

(Brickmaking machinery)

SHEVCHENKO, A. and I. Vinogradov (Pskov Oblast')

To Agriculture of the Northwest - a System of Machines"

Moscow, TASS, 9 Feb 1956

SHEVCHENKO, A.
[redacted]

For a new powerful expanskon of the physical-culture movement. Sov. profsoiuzy 4 no.9:8-13 S '56. (MIRA 9:10)

1. Sekretar' Vsesoyuznogo TSentral'nogo Soveta professional'nykh soyuzov. (Physical education and training)

SHEVCHENKO,A.

Our practices in ensiling. Zemeledelie 5 no.7:89 Jl '57.
(MLRA 10:8)

1. Starshiy agronom sovkhoza "Novaya Aleksandrovka."
(Ensilage)

SHEVCHENKO, A., red.; MATVEYEVA, A., tekhn. red.

[Conunterbores and counterboring] Zenkery i zenkovki. Moskva, Standartgiz, 1960. 61 p. (MIRA 14:5)
(Drilling and boring machinery)

SHEVCHENKO, A.

Machines take an examination. Znan. ta pratsia no.8:16-17
Ag '61. (MIRA 14:8)
(Agricultural machinery—Testing)

SHEVCHENKO, A., inzh.

For a greater variety of mixed feeds, Muk.-elev. prom. 27
no.11:14-15 N '61. (MIRA 14:12)

1. Otdel tekhnicheskogo razvitiya mukomol'no-krupyanoy i
kombikormovoy promyshlennosti Goskomiteta zagotovok Soveta
Ministrov SSSR.

(Feeds)

SHEVCHENKO, A.

Speck of dust is taken out. Znan.ta pratsia no.8:15 Ag '62.
(MIRA 15:12)

(Grain—Harvesting)

SHEVCHENKO, A. (UB5CLX) (Chernovtsy); BASOV, V. (Moskva); PRILUTSKIY, G. (Pyatigorsk); ARKHIPOV, Ye. (Bugul'ma); VYSOCHIN, V. (Moskovskaya obl.); PRIKHUNOV, I. (Moskovskaya obl.); OBLASOV, G. (Kiyev); SMIRNOV, Yu. (UA4YB) (Kanash); KHOKHLOV, B. (Moskva); KHALDEYEV, A. (Przheval'sk); SKOBELEV, I. (Primorskiy kray); PROSKUROV, V. (Irkutsk); DOBRYNIN, Yu. (g.Ivanovo /obl./)

Exchange of experience. Radio no.10:22,26,29,32,37,40,44,46,58 O '64. (MIRA 18:2)

ACC NR: AP6013414 (A) SOURCE CODE: UR/0317/65/000/009/0048/0051

AUTHOR: Shevchenko, A. (Lt. Gen.)

ORG: none

TITLE: Tank crew firing range

SOURCE: Tekhnika i vooruzheniye, no. 9, 1965, 48-51

TOPIC TAGS: military tank, artillery weapon, gunnery training

ABSTRACT: The author discusses the general problem of the all-around training of tank crews under conditions siumlating as closely as possible actual combat situations. Whereas natural-size firing ranges represent the optimal solution to the problem, it is argued that miniture proving grounds can also be a useful adjunct in the training program. One such range, having a shed-like structure 50 x 12 m, is described. In this set-up, training area No. 1 is a firing range where crews can practice stationary moving and close-in fire with 5.6-mm ammunition. In areas 2 and 3 there are additional facilities (platforms, screens indicating equipment, targets and associated target-shifting mechanisms) for fire training and for practice in managing the lifting and rotational mechanism (turret control devices) within the tank. Area 4 is devoted to fire training and gun-laying exercises. Working area 5 is set aside for training in tank assembly, disassembly and weapons study, and area 6 is essentially for radio communications training. Technical descriptions are given of the mechanical equipment

Card 1/2

ACC NR: AP6013414

(hit indicator, monitoring boards, mobile target carriage, etc.) employed in this facility. The range is located at one of the units of the Volga Military District. Orig. art. has: 5 figures.

SUB CODE: 15/ SUBM DATE: none

Card 2/2

SHEVCHENKO, A.

Depending on active members in labor. Mast.ugl. 6 no.5:18 My '57.
(MIRA 10:7)

1. Predsedatel' komissii po okhrane truda shakhty imeni Kirova kombinata Karagandaugol'.
(Coal mines and mining--Safety measures)

SHEVCHENKO, A.

In the interest of workers' rest and health benefits. Sov. profsoiuzy 16 no.10:14-17 My '60. (MIRA 13:6)

1. Sekretar' Vsesoyuznogo tsentral'nogo soveta profsoyuzov. (Trade unions) (Labor rest homes)

SMIRNOVA, A., kand. sel'skokhoz. nauk; SHABANOVA, M., kand. sel'skokhoz. nauk;
IONOVA, Z.; FED'KO, I., kand. biolog. nauk; SHEVCHENKO, A., aspirantka;
CHMYR', P., mladshiy nauchnyy sotrudnik

From work practices in the use of poisonous chemicals. Zashch. rast. ot vred. i bol. 10 no.3:22-24 '65. (MIRA 19:1)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut zashchity rasteniy (for Smirnova, Shabanova). 2. Nauchno-issledovatel'skiy institut sadovodstva im. I.V. Michurina, Michurinsk (for Ionova). 3. Vsesoyuznyy institut kukuruzy, Dnepropetrovsk (for Fed'ko). 4. Ukrainskiy institut rasteniyevodstva, selektsii i genetiki im. Yur'yeva (for Shevchenko).

SHEVCHENKO, A.A., kandidat tekhnicheskikh nauk.

Speed of wire drawing and the productivity of multiple wire-drawing machines. Stal' 7 no.2:131-134 '47. (MLRA 9:1)

1. Nauchno-issledovatel'skiy tekhnologicheskiy institut.
(Metal drawing) (Wire)

SHEVCHENKO, A.A., kandidat tekhnicheskikh nauk.

Kinematic and power data on piercing mills having variable angle inclined tapered rolls. Stal' 7 no.3:235-238 '47.
(MLRA 9:1)

1.Trubnyy institut.
(Rolling (Metalwork))

SHEVCHENKO, A. A.

SHEVCHENKO, A. A. -- "Elements of the Theory of Processes of Pressure Treatment of Bodies of Circular Section on Continuous-Operation Units." Sub 29 Jan 52, Inst of Metallurgy imeni A. A. Baykov (Dissertation for the Degree of Doctor in Technical Sciences)

So: Vechernaya Moskva, January-December 1952

SHEVCHENKO, A.A., doktor tekhnicheskikh nauk, professor; NIKOLAYEVSKIY, Yu.I., redaktor; ANDREYEV, S.P., tekhnicheskiy redaktor.

[Continuous rolling of pipes] Nepreryvnaia prokatka trub. Khar'kov. Gos. nauchno-tekhn. izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1954. 264 p. (MLRA 8:1)
(Rolling (Metalwork)) (Pipe)

YEMEL'YANENKO, Pavel Terent'yevich [deceased]; SHEVCHENKO, Aleksandr Andreyevich; AL'SHEVSKIY, L.Ye., redaktor; VALOV, N.A., redaktor; ATTOPOVICH, M.K., tekhnicheskiy redaktor

[Pipe rolling and pipe welding industry; textbook for schools and courses for foremen] Truboprokatnoe i trubosvarochnoe proizvodstvo; uchebnik dlia shkol i kursov masterov. Moskva, Gos. nauchno-tekhn. izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1954. 495 p.
(Pipe, Steel) (MLRA 8:1)

SHEVCHENKO, A.A., doktor tekhn.nauk

[redacted]

Elements in the theory of the continuous process of pipe rolling without mandrels. Obr.met.davl. no.3:164-189 '54. (MIRA 12:10)

(Rolling (Metalwork))

SOV/137-57-10-19178

Translation from: Referativnyy zhurnal, Metallurgiya, 1957, Nr 10, p 105 (USSR)

AUTHOR: Shevchenko, A.A.

TITLE: Re-examination of the Specifications for Tube Blanks With a View Toward Reduction of Rough Oversize and Limits (O peresmotre tekhnicheskikh usloviy na trubnyye zagotovki v storonu snizheniya pripuskov i dopuskov)

PERIODICAL: V sb.: Ratsionalizatsiya profiley prokata. Moscow, Profizdat, 1956, pp 272-274

ABSTRACT: Attention is called to the need for a re-examination of the specifications for machining blanks (B) in the direction of reducing rough oversize and limits. Until recently, the machine-manufacturing plants of the United States used tubular 245 mm B of 18-mm wall thickness, a diameter allowance of +2.5% and wall thickness limits of ± 15% for manufacturing cylinders of ~ 6-mm wall thickness. In the machining of these B, ~ 80% of the metal goes into the chip. By correcting the allowances for tube B, one may cut the chip scrap by more than 40%. Cold tube (T) rolling mills and draw benches are the equipments best suited to the manufacture of seamless tube. However, these

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SOV/137-57-10-19178

Re-examination of the Specifications for Tube Blanks (cont.)

equipments can be used only for the production of small-diameter T, up to 80 mm. The 1956-60 5-year Plan provides for the design and manufacture of mills in which cold rolling and drawing may be used to produce T up to 300 or 400 mm in size. Pilger mills, however, are the type best suited to the production of hot-rolled special-section T.

B.Ye.

Card 2/2

137-58-4-7203

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 4, p 126 (USSR)

AUTHORS: Rudoy, V.S., ~~Shevchenko, A. A.~~, Pishchikov, G. P., Belokurov, S. I., Stupel', S. I., Patlan', Ye. F., Chernyavskiy, A. A., Kholyavko, Z. I.

TITLE: Effect of External Defects in Steel Ingots on the Quality of Tubes Rolled on Pilger Mills (Vliyaniye naruzhnykh porokov stal'nykh slitkov na kachestvo trub, prokatyvayemykh na piligrimovykh ustanovkakh)

PERIODICAL: Byul. nauchno-tekhn. inform. Vses. n.-i. trubnyy in-t, 1957, Nr 3, pp 26-34

ABSTRACT: An investigation was made of ingots (I) of Nr 4 steel, 230 and 305 mm in diameter, exhibiting surface defects such as longitudinal cracks, twist, banding, and nonmetallic superficial inclusions. It was found that the rolling of I with cracks still present leads to the formation of scab on barrels (B) and tubes (T). Twists on I lead to the formation of through cracks or deep scab on B. The rolling of I having longitudinal cracks leads to the formation of shallow scabbing on B and T. The presence of banding results in the formation of fine transverse scab which burns out and be-

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137-58-4-7203

Effect of External Defects in Steel Ingots (cont.)

comes scale due to the insignificance of its dimensions. Accumulations of nonmetallic inclusions at the surface of the I leads to the formation of fine scab on the B and T. Flame repair of I having cracks up to 45 mm deep makes for production of up to 90 percent first class T, and rolling of I with banding to a depth of not over 30 mm yielded up to 95 percent first class T without repair. Rolling of banded I without repair and of I with cracks removed by the flame method makes it possible to save a considerable amount of metal that had previously been remelted.

I. M.

1. Steel--Processing--Effects of impurities 2. Steel tubing--Production 3. Steel tubing--Defects 4. Steel barrels--Production 5. Steel barrels --Defects

Card 2/2

SOV/137-59-2-4323

Translation from: Referativnyy zhurnal. Metallurgiya, 1959, Nr 2, p 284 (USSR)

AUTHORS: Shevchenko, A. A., Gulyayev, G. I., Yurgelenas, V. A.

TITLE: Stretch-reducing Operations on Welded Gas Pipes Without Subsequent Trimming of the Thickened Ends (Redutsirovaniye s natyazheniyem svarnykh gazoprovodnykh trub bez posleduyushchey obrezki utolshchennykh kontsov)

PERIODICAL: Byul. nauchno-tekhn. inform. Vses. n.-i. trubnyy in-t, 1958, Nr 4-5, pp 5-16

ABSTRACT: Stretch-reducing of welded gas pipes (P) from initial dimensions of 60x3.5 and 26.75x75 mm to 48 and 21.25 mm, respectively, was carried out in a two-high reducing stand equipped with individual motors which made it possible to ensure the necessary degree of stretching. Stretch reduction (SR) of the P's was accomplished in oval roll passes, the angular velocity of the rolls being so chosen that stretching by 4% was ensured in each roll stand. A total of four roll passes were calculated: Two roll passes, with an ellipticity of openings equivalent to 1.055 and 1.09, for the SR of P's from 60x3.5 to 48 mm, and two roll passes, with the same ellipticity, for SR of pipes from 26.75x2.75 mm

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SOV/137-59-2-4323

Stretch-reducing Operations on Welded Gas Pipes Without Subsequent (cont.)

to 21.25 mm. Experimental SR operations yielded the following results: 1) Welded gas P's fabricated by the furnace-welding process can be expediently worked by the SR method, 2) basic parameters were established for the operation of SR of welded gas P's in which the trimming of P ends is omitted; 3) it was established that neither the wall thickness and the variations in wall thickness along a transverse section, nor the quality of the weld in the gas P's are affected by the ellipticity of the oval passes; 4) a nine-stand, two-high SR mill with a common drive capable of imparting a 4% elongation to the pipe in each stand was found to be most rational.

Ye. T.

Card 2/2

SHEVCHENKO, A.A., doktor tekhn. nauk; GULYAYEV, G.I., kand. tekhn. nauk;
YURGELENAS, V.A., mladshiy nauchnyy sotrudnik; KITANENKO, V.P.,
inzh.; DERGACH, A.Ya., inzh.; ZUYEV, I.I., inzh.; KOROBOCHKIN, I.Yu.,
inzh.

Reduction of stretched thin-walled pipes. Biul. TSNIICHM no.4:
31-33 '58. (MIRA 11:5)
(Pipe) (Rolling (Metalwork))

S/137/60/000/011/025/043
A006/A001

Translation from: Referativnyy zhurnal, Metallurgiya, 1960, No.11, p.136, # 26363

AUTHORS: Shevchenko, A.A., Yurgelenas, V.A.

TITLE: The Intensifying of Tension When Reducing Pipes

PERIODICAL: Tr. Mezhvuz. nauchno-tekhn. kcnferentsii na temu: "Sovrem. dostizh. prokatn. proiz-va", Vol. 2, Leningrad, 1959, pp. 270 - 281

TEXT: The tension forces during hot rolling of pipes were determined with the aid of a specially developed and constructed device, which was placed between two heated pipes and passed together with the pipes through a 22-stand reduction mill with individual stand drive. The tension forces were perceived by ohmic resistance pick-ups, mounted in the recess of the device body. Heating of the device was prevented by a water-cooling system.

Ye.T.

Translator's note: This is the full translation of the original Russian abstract.

Card 1/1

VATKIN, Ya.L., kand. tekhn. nauk; SHEVCHENKO, A.A., doktor tekhn. nauk;
KRONFEL'D, I.D., inzh.; ROZHNOV, S.V., inzh.; CHEKMAREV, I.A., inzh.

Investigating the technology of pipe rolling on continuous mills with long mandrels. Obr. met. davl. no.5:143-164 '59.
(MIRA 13:3)

1. Dnepropetrovskiy metallurgicheskiy institut i Vsesoyuznyy nauchno-issledovatel'skiy trubnyy institut.
(Rolling (Metalwork))

S/137/61/000/006/040/092
A006/A101

AUTHORS: Shevchenko, A.A., Yurgelenas, V.A.

TITLE: Experimental determination of tensile force during hot reduction of pipes

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no. 6, 1961, 34-35, abstract 6D282 ("Byul. nauchno-tekhn. inform. Ukr. n.-i. trubn. in-t", 1959, no. 6-7, 5 - 15)

TEXT: The authors determined the tensile force on pipes being reduced in hot state on a 22-stand reduction mill from 98 x 3 mm to 76 mm diameter. For this purpose a device was employed which was mounted between 2 heated sleeves, rigidly connected with them and then passed through the reduction mill. This device may be used to measure the tensile force arising from the effect of stand no. 1, during the rolling of short sleeves, and also from the effect of several stands of the mill during the rolling of long sleeves. It is possible to measure the tensile force between both adjacent stands and stands vacated through one. For the measurements, short sleeves of 300 mm and long sleeves of 1,500 mm were used. During the first experimental measurements the 1,500 mm sleeves were

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21618

1.1300 also 1413, 1454

S/137/61/000/003/013/069
A006/A101

AUTHORS: Shevchenko, A.A., Gulyayev, G.I., Yurgelenas, V.A., Kitanenko, V. P., Dergach, A.Ya., Zuyev, I.I., Korobochkin, I.Yu.

TITLE: A technology of pipe reduction with tension

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no.3, 1961, 33, abstract 3D266 ("Byul. nauchno-tekhn. inform. Ukr. n.-i. trubn. in-t", no.6 - 7, 1959, 15 - 21)

TEXT: VNITI together with the Yuzhnotrubnyy Plant determined the parameters of pipe reduction with tension, in order to assist the pipe-rolling shops in assimilating the given technology. For the first time pipes of 57x2.75; 50x x2.75; 38 x 2.75; and 38 x 2.5 mm with ± 10% tolerances of wall thickness were obtained by hot rolling for the cold drawing shop. The authors investigated and recommended the grooving of rolls of the reduction mill with higher partial deformations.

K. U.

[Abstracter's note: Complete translation.]

Card 1/1

X

11300

24572

S/137/61/000/005/025/060
A006/A106

AUTHORS: Shevchenko, A.A., Rudoy, V.S., Chernyavskiy, A.A.

TITLE: Production of pipes of variable section on a pilger mill

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no.5, 1961, 29, abstract 5D267 ("B'yul. nauchno-tekhn. inform. Ukr. n.-i. trubn. in-t", 1959, no. 6 - 7, 26 - 28)

TEXT: Pipes of variable section were rolled from sleeves produced on a piercing mill and from a pipe blank prerolled on a pilger mill on special shaped mandrels. It is concluded that pilger mills can be used to produce large diameter pipes with walls thickened at the ends and shaped over the length; the ratio of the wall thickness in the thickened portion to the basic section is up to 2 - 3; the length of the thickened portion is limited by the weight of the ingot. The mechanical properties of the pipe remain approximately constant over the whole length of the pipe. This is connected with the absence of curvature and bending of the metal threads. Metal folds, formed during rolling on the transition spots

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Production of pipes of variable section on a pilger mill S/137/61/000/005/025/060
A006/A106

of the thickened wall to the basic pipe section do not reduce the mechanical properties of the pipe and may be easily eliminated by internal boring.

Yu. M.

[Abstracter's note: Complete translation]

Card 2/2

S/137/61/000/002/041/046
A006/A001

Translation from: Referativnyy zhurnal, Metallurgiya, 1961, No. 2, p. 16 # 2I125

AUTHORS: Shevchenko, A.A., Alferova, N. S., Rudoy, V. S., Kutsenko, G. F., Nesterova, N. N., Konovalov, V. P.

TITLE: Properties and Structure of High-Manganese Austenite 45Г17Ю3 (45G17Yu3) Steel

PERIODICAL: "Byul. nauchn. tekhn. inform. Ukr. n.-i. trubn. in-t". 1959, No. 8, pp. 17-26

TEXT: The authors investigated the ductile properties of 45G17Yu3 steel composed of (in %): C 0.4 - 0.5; Mn 16 - 18; Al 3.5 Si $\leq$ 0.6. It was found that the 45G17Yu3 steel was characterized by a sharply pronounced microchemical heterogeneity. The temperature of the beginning fusion of metal grains of the blank was 1300 - 1350°C (depending on the method of manufacture). Optimum ductility of 45G17Yu3 steel for hot deformation conditions in diagonal rolling mills corresponds to a temperature of 1200°C. The metal of the investigated 45G17Yu3 steel melts shows highly heterogeneous properties. Ductile properties of the blanks from different plants, melts and of bars from the same ingot are highly

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BELYKH, K.D., inzh. (Dneprodzerzhinsk); SEGEDA, S.B., inzh. (Dneprodzerzhinsk); SHEVCHENKO, A.A., starshiy dorozhnyy master (Dneprodzerzhinsk)

Track maintenance workers of a metallurgical plant. Put' i put. khoz. no.12:25-26 D '59. (MIRA 13:4)

1. Nachal'nik sluzhby puti Metallurgicheskogo zavoda im. F.E. Dzerzhinskogo (for Belykh). 2. Zamestitel' nachal'nika sluzhby puti Metallurgicheskogo zavoda im. F.E.Dzerzhinskogo, (for Segeda).
(Dneprodzerzhinsk--Industrial railroads)

S/137/62/000/001/088/237
A052/A101

AUTHORS: Shevchenko, A.A., Strizhak, V.I.

TITLE: Production of pipes with improved mechanical properties for the petroleum and gas industry

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no. 1, 1962, 34, abstract 1D221 (Metallurg. i gornorudn. prom-st', Nauchno-tekhn. sb., no. 4, 1960, 36 - 38)

TEXT: To satisfy the needs of the gas and petroleum industry during the seven-year-plan period, drilling and drive pipes of improved design with σ_s [illegible] 100 kg/mm^2 will be required. This can be achieved either by raising the strength characteristics or by improving the threaded couplings with equalized strength of the pipe body and the coupling. σ_s of drilling and drive pipes provided for by the USSR standards varies from 38 to 75 kg/mm^2. At present the production of pipes with the minimum σ_s value of 55 kg/mm^2 (E grade) is realized. Owing to the absence at the pipe plants of equipment necessary for a complex heat treatment, the strength characteristics are raised by applying alloyed steels which results in expensive pipes. UkrNITI carried out works on application for

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the high-strength pipes of medium-carbon steel grades Ст 40Х (St40Kh) and 36Г2С (36G2S) with subsequent tempering, which have σ_s of 65 and 75 kg/mm^2 respectively. Deeper wells and increased pressure in them require improved designs of pipe couplings. Such pipes are produced with upset lock ends. Two technological variants for production of these pipes are proposed. The Kramatorsk NIIPTMash provides for the manufacturing of pipes with thickened ends by means of a continuous jolting of inductor-heated metal. UkrNITI proposed a technology of production with upset lock ends providing for the deformation divided between the pilger mill and heading presses. An approach to the solution of the problem of producing lock end pipes is the welding of lock couplings to pipes. The technology of production of such pipes, developed and realized at the Plant imeni Andreyev, is described.

Ye. Krichevskiy

[Abstracter's note: Complete translation]

S/133/61/000/003/009/014
A054/A033

AUTHORS: Shevchenko, A. A., Doctor of Technical Sciences; Gulyayev, G. I. Candidate of Technical Sciences; Anisiforov, V. P., Candidate of Technical Sciences; Arutyunov, I. G., Candidate of Technical Sciences; Yurgelenas, V. A., Engineer, and Fedin, V. P., Engineer

TITLE: The performance of two-high reducing mills with individual drive

PERIODICAL: Stal', no. 3, 1961, 251 - 256

√

TEXT: When planning three-high reduction mills, the VNIITMETMASh and UkrNITI made a thorough study of the two-high reduction mills with individual drive, not supplied with rotation-stabilizers. In order to match the operation of these two types of mills the single deformation values were taken a little higher ($m_i = 3.5 \div 4.2$ %) than usual in Soviet plants. The tube dimensions varied between 96 x 3.25 - 3.5; 96 x 4 - 4.5 and 96 x 5 mm. The motor speeds for these types of tubes are given in table 2. Before reduction the tubes were heated to 1040 - 1080°C, the number of motor revolutions was recorded on the switchboard by means of an MM type tachovolt-

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meter with a relatively low accuracy (± 10 rpm). The data compiled for the average change in wall-thickness at the end and central parts of the tubes rolled in 21 and 17 stand mills are given in tables 3 and 4. They show that when the tension is increased the wall-thickness in the central part of the tube decreases, while the increase in wall-thickness at the tube ends will reach a maximum only at tensions of 0 - 0.5 %. In all other cases any increase in tension reduces the wall-thickness at the tube ends. Table 4 shows that the deviation in wall-thickness in lateral direction suddenly increases at the ends, irrespective of the tension, while it decreases in the central parts, when the tension is raised. With templates of 96 x 4 and 96 x 5 mm tubes it was established that the transverse section remains fairly stable even when no tension at all was applied, whereas the 96 x 3.25 mm tubes displayed defects (beads and fractures) when reduced without tension, by 5.4 and 7 %. When applying a tension of 3.5%, no defects were observed in the walls of the 96 x 3.5 mm tubes. The values of kinematic tension of 3.5 % in the 21-stand and of 4% in the 17-stand mills does not represent the limit. Experiments showed that it was possible to increase the kinematic tension and to produce tubes with even thinner walls in the central parts. If the tubes are rolled at the right temperature and the roll speed adjusted carefully, the coefficient of tension can be as high as 0.7 - 0,8 (Ref. 7: G.I. Gulyayev; V. A. Yurgelenas: Determination of Some Basic Technological Parameters of Tube Reduction with Tension. Transactions of the UkrNTO ChM, 1958, vol. 13). Tests carried out to establish the maximum values of torques and those for stabilized operation show that the torque values characterize the non-uniform load of the stands which in the first place depends on the adjustment of the roll-speed. When the tension is increased from 3.5 to 4%, the torques of the middle-stand motors decrease uniformly, once the rolling process has been stabilized. The tests also proved that in the experimental reductions the motors were not always loaded to full capacity, while overloading also occurred due to the inaccurate adjustment of the revolution of rolls, (n). When calculating the reduction of the mills, depending on the tension applied, the wall-thickness of the tube and partial deformation obtained in one stand have to be taken into account. The oscillogramm of current intensity shows that, at the rate at which the tube proceeds to the next stand, the current intensity curve declines, under the effect of the frontal tension of the following stand. This step-like character of the de-

✓

crease in current intensity indicates the moment, when the tube enters the next stand. When the tension at the rear (viewed from the preceding stand) is taken as constant, the maximum stretching force will be proportionate to the difference of the ordinates of the maximum and stabilized values of the current. The decrease in the general moment from the maximum to stabilized state will be proportionate to the moment acting on the stand investigated from the next following stand:

√

$$\Delta M_{gen} = TD_r \quad (1)$$

$$T = k \Delta I \quad (2)$$

$$\Delta I = I_{max} - I_{stab} \quad (3)$$

$$k = \frac{v}{1.03\, n_{i.r} \cdot D_r} \quad (4)$$

where M_{gen} = general moment, k = coefficient of proportionality, v = vol-

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A054/A033

The performance of two-high reducing ...

tage, v, D_r = rolling diameter of the roll, mm, $n_{i.r}$ = velocity of idle run of rolls, rpm, T = stretching force, kg, I_{max} and I_{stab} = current intensities for maximum and stabilized moments, a. ABSTRACTER'S NOTE: subscripts gen. (general), r(rolling), i.r. (idle run), stab. (stabilized) are translations of the original об (obshchyy), к (katayushchyy), хх (kholostoy khod) and уст (ustanovlenyy) . Based on these formulas it is possible to calculate the actual stretching forces and longitudinal stresses in the tube on the stand, when being reduced at different tensions and various initial wall-thicknesses. The distribution of forces and stresses of tension has no regular character; e.g., the maximum value of tension stress is 3.6 kg/sq mm (practically the yield point of the metal processed) while at a tension of 3.5 % it amounts to 2.6 kg/sq mm and at 4 % to 1.8 kg/sq mm. The maximum stretching force attains 2100 kg. The difference in stretchingforces for the various stands of the mill are, to a certain extend, caused by the inaccurate adjustment of the rolls. The investigation of roll-speed shows that there is a deviation between the actual and the rated speed of the rolls, both in idle run and in operation. In some cases the speed increases for the subsequent rolls, sometimes, however, a

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1

decelaration is observed. The velocity drops on successive rolls affects the reduction process in several aspects: energy consumption, torques, forces, tension, etc. Therefore the correct adjustment of the number of roll revolution in stands with individual drive is of great importance, because variations in the roll speed result in an irregular change of energetic parameters, which unfavourably affects the tube quality. The tube walls will not be of uniform thickness and cracks may occur even at relatively low tensions. There are 5 figures, 4 tables and 8 references: 7 Soviet, 1 non-Soviet.

ASSOCIATION: UkrNITI, VNIIMETMASh

Table 2: ① Rotation speed of electromotors p.m. at the reduction of tubes to 38 mm from 96 x 3, 96 x 4 and 96 x 5 mm, (A, B, C); ② No. of stand; ③ Reduction in the 21-stand mill; ④ Reduction in the 17-stand mill; ⑤ A B C; ⑥ A B C; ⑦ Rotation speed of motor, rpm, at tension of med,%; ⑧ The power of each motor: 36 kw, the range of revolutions 500-- 1000 min., the transmission value of reducers for stands 1 - 6 : 12,696;

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The performance of two-high reducing ....

Table 2 (continued)
stands 7 - 1:10,843;
stands 12 - 15:8,912;
stands 16 - 19:7,754;
stands 20 - 22:6,779.

① Скорость вращения электродвигателей (об/мин) при редуцировании до диаметра 38 мм труб размером 96×3 (А), 96×4 (Б) и 96×5 (В) мм Table 2

② № клети	③ Редуцирование в 21 клети*						③ Редуцирование в 17 клетях*					
	А	④		Б; В			А	④		Б; В		
	⑤ скорость вращения двигателей, об/мин, при натяжении $\varepsilon_{ср}$, %											
	0,0	2,0	3,5	0,0	2,0	3,5	0,0	2,0	3,5	0,5	2,5	4,0
2	700	500	500	700	500	500	—	—	—	—	—	—
3	708	516	523	709	517	524	—	—	—	—	—	—
4	715	532	548	716	532	548	—	—	—	—	—	—
5	725	549	574	727	551	575	—	—	—	—	—	—
6	735	568	603	736	570	603	800	750	600	800	650	575
7	637	502	540	637	503	604	691	660	539	698	579	519
8	651	523	571	653	526	640	700	683	568	714	603	550
9	666	545	604	670	550	680	714	709	601	735	633	585
10	681	569	640	689	577	723	735	745	643	765	671	629
11	699	595	679	709	605	770	760	785	691	798	714	680
12	589	512	593	601	523	675	646	682	611	686	627	605
13	606	536	630	620	551	722	671	722	659	718	670	656
14	623	562	671	642	581	773	698	766	712	754	717	712
15	641	590	715	666	614	829	728	815	773	794	771	776
16	577	541	666	603	568	777	662	756	732	730	722	738
17	596	570	712	628	603	837	691	806	795	769	775	805
18	616	601	761	656	642	904	726	863	868	815	839	883
19	637	634	815	686	[illegible]	978	763	925	950	866	909	971
20	577	585	763	637	[illegible]	[illegible]	702	868	909	805	862	933
21	581	601	795	643	666	981	706	890	950	817	892	979
22	581	601	795	643	666	981	706	890	950	817	892	979

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* Мощность каждого двигателя 36 квт при регулировании числа оборотов от 500 до 1000 в минуту. Передаточное число редукторов 1—6-й клетей составляет 12,696, 7—11-й — 10,843, 12—15-й — 8,912, 16—19-й — 7,754 и 20—22-й клетей — 6,779.

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The performance of two-high reducing ...

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A054/A033

Table 3: ① Change in average wall-thickness of tubes reduced in 21-stands from 96 x 3.25, 96 x 4 and 96 x 5 mm to 38 mm at single deformation of 5.4 %; ② Tension, %; ③ Tube wall-thickness, mm; ④ Before reduction; ⑤ After reduction actual; ⑥ Change in wall-thickness, mm; ⑦ Place of measuring; ⑧ calculated; ⑨ actual; ⑩ П = F, frontal part of tube, C = C, central part of tube; З = R, rear part of tube.

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TABLE 3

① Изменение средней толщины стенки труб, редуцированных 21 клети с размеров 96×3,25; 96×4 и 96×5 мм до 38 мм пр частных деформациях до 5,4%

Натяжение, % ②	③ Толщина стенки трубы, мм			Изменение толщины стенки трубы мм ⑥	Место замера* ⑦
	④ до редуцирования		после редуцирования (фактическая) ⑤		
	номинальная ⑧	фактическая ⑨			
0,0	3,25	3,39	5,13	+1,74	П
		3,30	4,42	+1,12	С
		3,21	4,69	+1,48	З
2,0	3,25	3,34	4,47	+1,13	П
		3,24	3,16	−0,08	С
		3,13	4,36	+1,23	З
3,5	3,25	3,31	4,20	+0,89	П
		3,25	2,71	−0,54	С
		3,20	4,45	+1,25	З
0,0	4,0	4,10	5,99	+1,89	П
		4,00	5,00	+1,00	С
		3,90	5,77	+1,87	З
2,0	4,0	3,87	5,68	+1,81	П
		3,88	3,75	−0,13	С
		3,89	5,52	+1,63	З
0,0	5,0	4,95	7,33	+2,38	П
		4,88	6,22	+1,34	С
		4,81	7,06	+2,25	З
2,0	5,0	5,05	6,92	+1,87	П
		4,98	4,71	−0,27	С
		4,92	7,05	+2,13	З

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⑩ * П — передний конец трубы; С — середина трубы; З — задний конец.

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A054/A033

Table 4:

① Изменение средней толщины стенки труб, редуцированных в 17 клетях с размеров 96×3,5; 96×4—4,5 и 96×5 мм до 38 мм при частных деформациях до 7%

Таблица 4

② Натяжение, %	Толщина стенки, мм			Изменение толщины стенки трубы, мм	Поперечная разностенность, мм			Место замера*
	до редуцирования		⑤ после редуцирования (фактическая)		до редуцирования	после редуцирования	изменение	
	⑥ номинальная	⑦ фактическая						
0,0	3,5	3,53	5,57	+2,04	0,62	1,50	+0,88	П
		3,41	4,45	+1,04	0,40	1,50	+1,10	С
		3,29	4,75	+1,46	0,27	1,54	+1,27	З
2,0	3,5	3,36	4,78	+1,42	0,30	0,93	+0,63	П
		3,39	3,38	—0,01	0,26	0,47	+0,21	С
		3,42	4,52	+1,10	0,23	1,46	+1,23	З
4,0	3,5	3,41	4,55	+1,14	0,62	0,88	+0,26	П
		3,34	2,89	—0,45	0,52	0,48	—0,04	С
		3,27	4,73	+1,46	0,42	1,34	+0,92	З
0,5	4,5	4,78	6,86	+2,08	0,50	0,66	+0,16	П
		4,67	5,38	+0,71	0,37	0,75	+0,38	С
		4,55	6,65	+2,10	0,25	1,46	+1,21	З
2,5	4,0	3,82	5,48	+1,66	0,34	0,95	+0,61	П
		3,78	3,61	—0,17	0,45	0,53	+0,08	С
		3,73	5,43	+1,70	0,56	1,63	+1,07	З
4,0	4,0	4,18	5,78	+1,60	0,33	1,69	+1,36	П
		4,09	3,54	—0,55	0,31	0,41	+0,10	С
		4,00	5,74	+1,74	0,29	1,61	+1,32	З
0,5	5,0	4,86	7,10	+2,24	0,64	1,82	+1,18	П
		4,92	5,77	+0,85	0,57	0,69	+0,12	С
		4,99	7,28	+2,29	0,51	1,79	+1,28	З
4,0	5,0	5,07	6,83	+1,76	0,78	1,17	+0,39	П
		4,98	3,98	—1,00	0,58	0,55	—0,03	С
		4,90	7,01	+2,11	0,38	1,98	+1,60	З

* П— передний конец трубы; С—середина трубы; З—задний конец.

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A054/A033

The performance of two-high ....

Table 4 (continued) ① Change in the average wall-thickness of tubes reduced in 17-stands from 96 x 3.5, 96 x 4 - 4.5 and 96 x 5 mm to 38 mm, at single deformations of 7 %; ② Tension, %; ③ Wall-thickness, mm; ④ Before reduction; ⑤ After reduction (actual); ⑥ calculated; ⑦ actual; ⑧ Change in wall-thickness, mm; ⑨ Lateral deviation in wall-thickness, mm; ⑩ Before reduction; ⑪ after reduction; ⑫ Change; ⑬ Place of measuring; ⑭ П = F, frontal part of tube, С = C, central part of tube, З = R, rear part of tube.

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S/133/62/000/007/009/014
A054/A127

AUTHORS: Shevchenko, A.A., Doctor of Technical Sciences; Gulyayev, G.I., Candidate of Technical Sciences; Zimin, A.K., Engineer

TITLE: The effects of the heating temperature and chemical composition on the changes in the wall-thickness of tubes during reduction

PERIODICAL: Stal', no. 7, 1961, 632 - 633

TEXT: At the UkrNITI tests were carried out with 180-mm long and 50-mm external diameter machined tubes of 10 (10) and 1Х 18Н 9Т (1Kh18N9T) steels with heating in an electric furnace in an argon atmosphere and reduction on a 7-stand double-roll mill (with 160-mm diameter rolls). After reduction the tubes were immersed in water, scale could therefore develop only for a short time, i.e., during feeding to the mill and rolling (25 - 45 sec). At 50 mm from the tube end annular notches were made on which the wall thickness was marked (at six points before and 12 points after reduction). The tests were carried out at 800,-900, 1,000, 1,100 and 1,200°C. The effect of the chemical composition was studied on tube branches 50 mm long, with a wall-thickness of 4.5 mm, while reducing them

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SHEVCHENKO, A.A., doktor tekhn.nauk; GULYAYEV, G.I., kand.tekhn.nauk;
ANISIFOROV, V.P., kand.tekhn.nauk; ARUTYUNOV, I.G., kand.tekhn.nauk;
YURGELENAS, V.A., inzh.; FEDIN, V.P., inzh.

Peformance of a two-high reduction mill with individual drive.
Stal' 21 no.3:251-256 Mr '61. (MIRA 14:6)

1. Ukrainskiy nauchno-issledovatel'skiy trubnyy institut i
Vsesoyuznyy nauchno-issledovatel'skiy institut metalloobrabotki
i mashinostroyeniya.
(Rolling mills)

SHEVCHENKO, A.A., doktor tekhn.nauk; GULYAYEV, G.I., kand.tekhn.nauk; ZIMIN, A.K., inzh.

Effect of the temperature of heating and chemical composition of the metal on changes in pipe wall thickness during their reduction. Stal' 22 no.7:632-633 Jl '62. (MIRA 15:7)

1. Ukrainskiy nauchno-issledovatel'skiy trubnyy institut.
(Pipe mills)

S/124/63/000/003/054/065
D234/D308

AUTHORS: Shevchenko, A. A. and Zimin, A. K.

TITLE: Stability of the cross-section of a pipe during rolling on two- and three-roller reduction mills

PERIODICAL: Referativnyy zhurnal, Mekhanika, no. 3, 1963, 35, abstract 3V246 (In collection: Proiz-vo trub no. 7, Khar'kov Metallurgizdat, 1962, 51-64)

TEXT: The authors consider the formation of necks in reduced pipes, due to loss of stability of the cross-section in rolling. On the basis of a formula giving the loss of stability of a rectangular plate, the authors make conclusions regarding the qualitative effect of dimensions, cogging, the magnitude of the gap between the rollers, number of rollers constituting the pass, as well as the significance of tension during the reduction of pipes. The experimental dependence is given of the critical deformation of the pipe on the ratio of pipe diameter to wall thickness in reduction without tension in two- and three-roller oval passes, ob-

Card 1/2

SHEVCHENKO, A. A.; KLINOV, I. Ya.

Long-period strength of glass plastics under the action of a corrosive medium and temperature. Plast. massy no.11:41-43 '62. (MIRA 16:1)

(Glass reinforced plastics—Testing)

SHEVCHENKO, A.A.

Technique of determining the stress-rupture strength and creep of glass plastics in a corrosive medium. Zav. lab. 29 no.10:1249 '63. (MIRA 16:12)

1. Moskovskiy institut khimicheskogo mashinostroyeniya.

SHEVCHENKO, A.A. (Kalinin, 1-ya Perevolotskaya ultisa, 40, kvartira 13)

Innervation of the skin of the gluteal region. Arkh. anat., gist. i embr. 45 no.7:72-76 Je '63. (MIRA 17:4)

1. Kafedra normal'noy anatomii (zav. - prof. I.S. Kudrin) Kalininskogo gosudarstvennogo meditsinskogo instituta.

L 51985-65 EPA(s)-2/EWT(m)/EPF(c)/EPR/EWP(j)/T Pc-4/Pr-4/Ps-4/Pt-7
RM

ACCESSION NR: AT5012209 UR/3078/64/028/000/0165/0183

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41
B+1

AUTHOR: **Shevchenko, A. A.**

TITLE: Temperature -time dependence of the strength of fiberglass reinforced plastics in some aggressive media

SOURCE: Moscow. Institut khimicheskogo mashinostroyeniya. Trudy, v. 28, 1964. [illegible] khimicheskoy apparatury (Corrosion of chemical apparatus), 165-183

[illegible] fiberglass, reinforced plastic, plastic strength, plastic corrosion, [illegible] glass fiber laminate, polyester resin

ABSTRACT: The author studied the effect of load, temperature, and corrosive medium on the epoxide-phenolic glass-fiber laminate EF-32-301, polyester resin glass-fiber laminate PN-1, and furyl resin glass-fiber laminate FL-1. The cor[illegible] sulfuric acid (3, 30, 60%) and sodium hydroxide (1, 10, 20%). [illegible] tests were carried [illegible] the samples in these solutions. Three [illegible] evaluating the chemical stability were employed: (1) stress applied [illegible] of rupture, (2) loss of strength due to exposure under stress, and (3) loss of strength due to exposure without load ("standard method"). When [illegible] data were plotted in the semilogarithmic coordinates σ vs. log τ (where σ is the stress at rupture and τ is the time preceding rupture), straight lines were

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produced for both the acid and alkaline solutions (for a wide range of temperatures, the temperature being constant). The equation of the straight lines is $\tau = A e^{-\alpha\sigma}$, where A and α are parameters which determine the time dependence of the strength of the material on the prevailing conditions. Methods of determining α and A for various temperatures are described. Orig. art. has: 14 figures, 5 tables, and 7 formulas.

ASSOCIATION: Moskovskiy institut khimicheskogo mashinostroyeniya (Moscow Institute of Chemical Machine Building)

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AUTHOR: **Shevchenko, A. A.; Bokshitskaya, N. A.**

TITLE: Methods for corrosion testing of plastics 15

SOURCE: Moscow. Institut khimicheskogo mashinostroyeniya. Trudy, v. 28, 1964. Korroziya khimicheskoy apparatury (Corrosion of chemical apparatus), 232-237

TOPIC TAGS: plastic corrosion, corrosion resistance, fiberglass, reinforced plastic, polyethylene, corrosion testing

ABSTRACT: To determine the behavior of plastics under various testing conditions, the authors studied three types of fiber-glass reinforced plastics (EF-32-301, PN-1, and FL-1) and low- and high-pressure polyethylene in aqueous solutions of sulfuric acid and sodium hydroxide by three different methods: (1) the "gravimetric" or "standard" method - change in tensile strength after keeping the specimens in the aggressive medium without load; (2) keeping the specimens in the medium under a constant tensile load at various temperatures, washing, drying, and testing for tensile strength; (3) testing the materials under a constant tensile load at a high temperature and in an aggressive medium until rupture occurred. Durability curves were plotted on the basis of the results. The data obtained by the three methods exhibit substantial differences, particularly

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between the first and the third method. An analysis of these results shows that the "standard" method is not satisfactory for evaluating plastics as structural materials, because it does not reproduce the conditions characteristic of the operstion of such parts in chemical apparatus, namely, the simultaneous action of load, temperature, and an aggressive medium. The third method is much more appropriate for such purpures. Orig. art. has: 3 figures and 2 tables.

ASSOCIATION: Moskovskiy institut khimicheskogo mashinostroyeniya (Moscow Institute of Chemical Machine Building)

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BUDNIK, N.M., kand. tekhn. nauk; SHEVCHENKO, A.A., inzh.; DYURGEROV, N.G.;
SAPOV, P.M., inzh.; BARILOV, O.A.; NAKHIMOVICH, E.I.

Reconditioning shafts by build-up welding with a short arc.
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(MIRA 17:11)

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MATSELYUKH, B.P.; SHEVCHENKO, A.A.; PAVLENKO, N.I.

Comparative physicochemical characteristics of high polymer deoxyribonucleic acids in actinomycetes and Bacillus breslavensis. Mikrobiologiia 34 no.4:590-597 Jl-Ag '65.

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S/191/62/000/011/010/019
B101/B186

AUTHORS: Shevchenko, A. A., Klinov, I. Ya.

TITLE: Fatigue strength of glass plastics under the action of an aggressive medium and of temperature

PERIODICAL: Plasticheskiye massy, no. 11, 1962, 41-43

TEXT: An apparatus (Fig. 1) for testing the fatigue strength of glass plastics under the action of aggressive solutions and at elevated temperatures is described. ЭФ-32-301 (EF-32-301) epoxy phenol glass textolite (I) and glass textolite based on ПН-1 (PN-1) polyester resin (II) filled with $Т_1$ (T_1) glass fabric were tested. Results: (1) In 20% NaOH, at 650 kg/cm^2 stress (15% of the tensile strength) and at room temperature, the strength of I decreased by 60% after 5000 hrs. Without stress, but after 1000 hrs at 50°C, 800 hrs at 20°C, the strength dropped by 65% in this solution. (2) In 30% H_2SO_4, the durability of I at 90°C was only 1/32 of the durability at 50°C, but the durability-versus-stress curves in this acid were similar for both these temperatures. At room temperature,

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the strength dropped by 30% after 1800 hrs. (3) In 30% H_2SO_4, at 620 kg/cm^2 stress and 20°C, II started decomposing after 200 hrs, but at 50°C it did so after only 2 hrs. Without stress, the strength at 50°C dropped by 43% after 200 hrs. The glass textolite II is stable to H_2SO_4 at room temperature only. (4) The deformation - stress relation follows Hooke's law. No flowing occurs, and the fracture is brittle. There are 4 figures.

Fig. 1. Apparatus for testing glass plastics in stressed state.
Legend: (1) Lever arrangement; (2) clamps; (3) clamping jaws; (4) rubber stoppers; (5) small weights; (6) glass plastic specimen; (7) glass vessel; (8) frame; (9) to return-flow cooler.

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SHEVCHENKO, A.A.; BOKSHITSKAYA, N.A.

Method for corrosion testing of plastics. Trudy MIKHM 28:
232-237 '64. (MIRA 19:1)

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Effect of temperature and time on the strength of glass plastics in some aggressive media. Trudy MIKHM 28: 165-183 '64. (MIRA 19:1)

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Results of herbicide testing. Zashch. rast. ot vred. i bol. 9 no.7:23-26 '64. (MIRA 18:2)

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IGNATUSHCHENKO, K.G.; SHEVCHENKO, A.F.

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(Building)